

Transforming Power Transmission: The Advantages of Magnetic Gears

Magnetic Gear

Mechanical gears, traditionally used for speed and torque adjustment in various applications, face issues like friction and noise, impacting their efficiency and reliability. Magnetic gears emerge as a superior alternative, offering frictionless, non-contact power transmission. This innovation leads to reduced maintenance, minimized heat generation, and inherent overload protection, enhancing safety and operational efficiency. They are increasingly favored in applications requiring high safety, clean environments, and efficient power mobility, such as electric vehicles and industrial machinery. With diverse designs like coaxial and parallel axial, magnetic gears represent a significant advancement in gear technology.

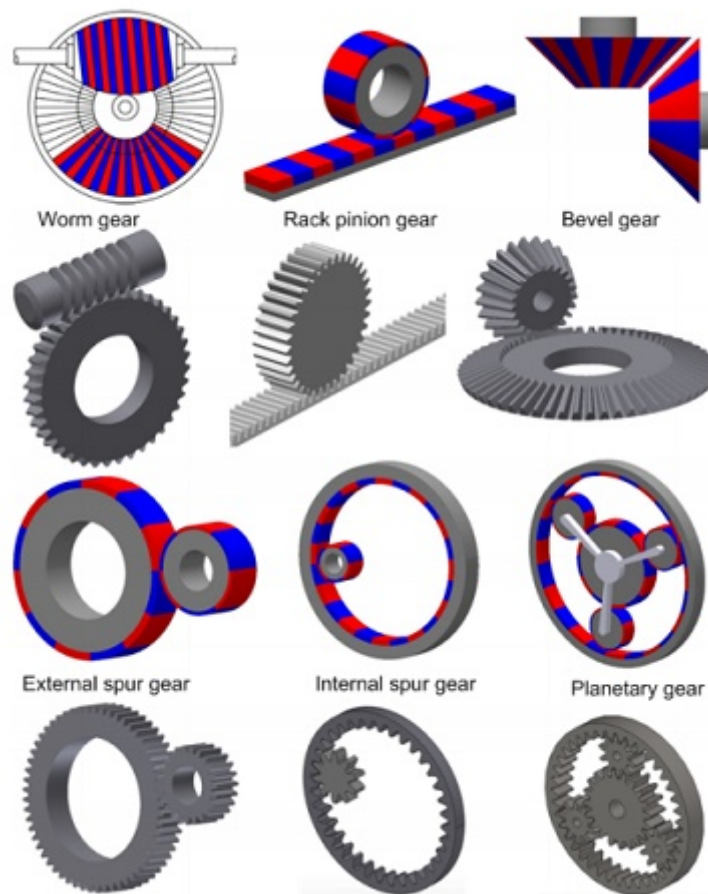


Figure 1 - Magnetic gear topologies

Magnetic gears offer benefits but face challenges like size and cost. Efforts aim to enhance torque density and reduce size and costs. The finite element method (FEM) is reliable for engineering system design and analysis, especially in simulating complex geometries. EMWorks2D specializes in magnetic and electric problem-solving, providing accurate 2D solutions. This study uses EMWorks2D to analyze the magnetic

properties of two coaxial magnetic gear models, comparing torque results with references for validation.

2D simulation of coaxial magnetic gear [2]

A coaxial magnetic gear model with an inner rotor comprising $P_i=2$ pole-pairs and an outer rotor with $P_o=3$ pole-pairs, along with $Q=5$ ferromagnetic pole-pieces, is detailed in [2]. The inner rotor, termed high-speed (HS), rotates faster than the outer rotor, designated low-speed (LS). Despite the HS rotor's higher speed, the LS rotor generates greater torque. Using EMWorks2D, magnetic flux, and torque are assessed in the air gap region, with end effects disregarded. Iron core permeability is infinite, while magnets possess a remanence of 1.2T and a relative permeability of 1, featuring alternating radial magnetization. Table 1 summarizes the model's key properties, with Figure 2 depicting the 2D model.

Table 2 - Main properties of the MG

Items	Value
Radius of the inner rotor yoke	40.00 mm
Outer radius of the inner rotor PMs	50.00 mm
Inner radius of the slots	52.00 mm
Outer radius of the slots	62.00 degree
Slot opening	36.00 deg
Inner radius of the outer rotor PMs	64.00 mm
Inner radius of the outer rotor yoke	74.00 mm
Axial length	100.00
Pole-pairs inner rotor	2
Pole-pairs outer rotor	3
Ferromagnetic pole-pieces	5

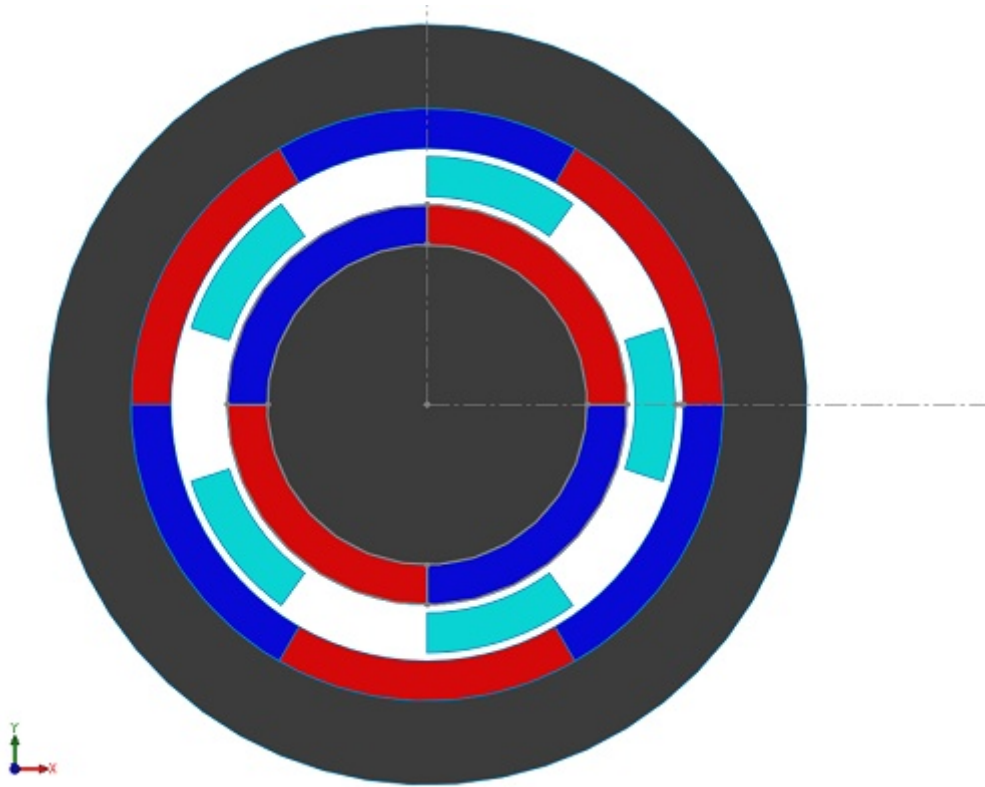


Figure 2 - 2D model of the simulated magnetic gear system

EMWorks2D features an automatic and adaptable mesher, producing triangular mesh elements. Mesh refinement, specifically targeting the air gap region, ensures precision in results. Figure 3 illustrates the mesh plot generated by EMWorks2D.

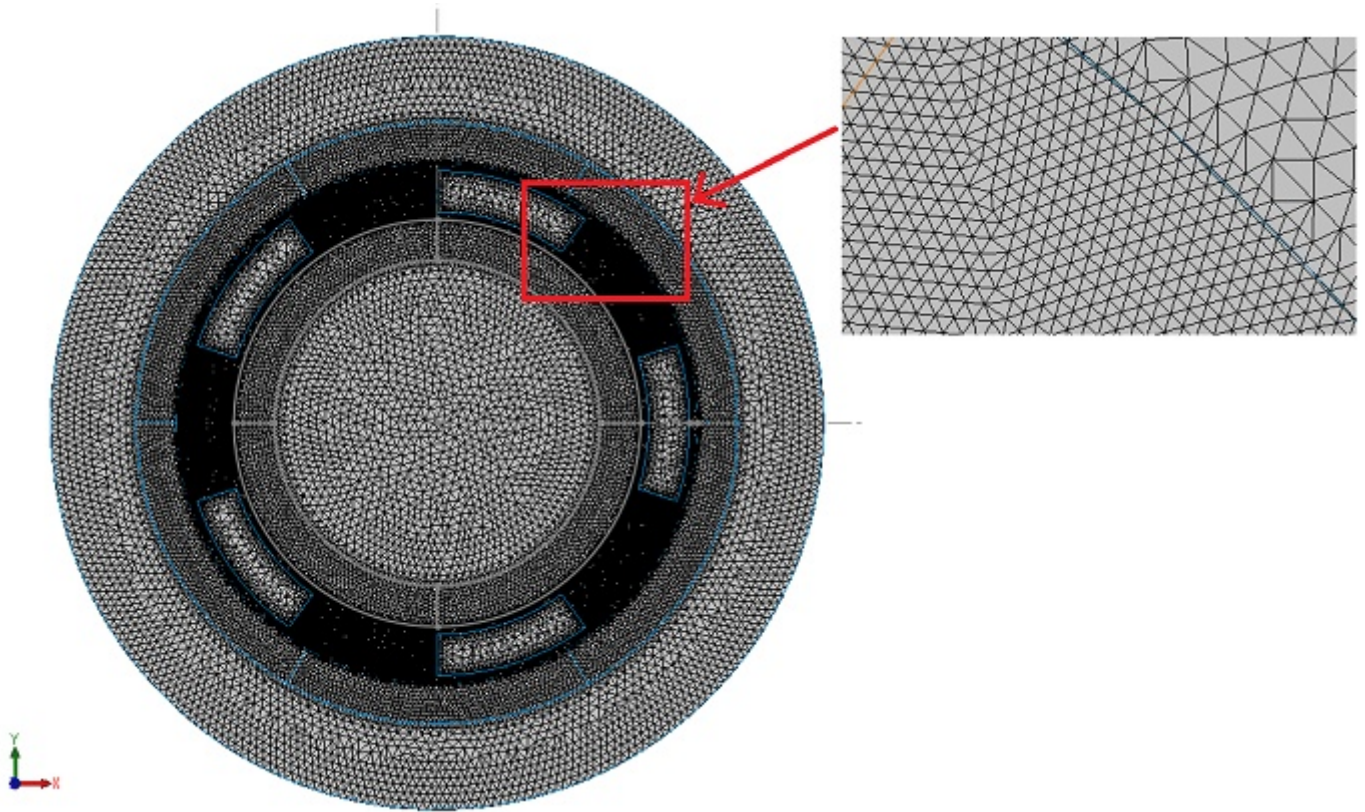
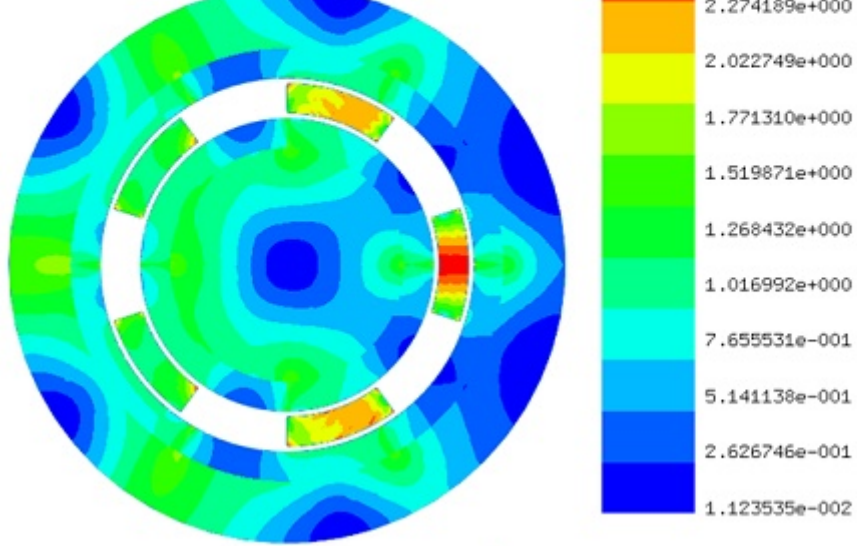
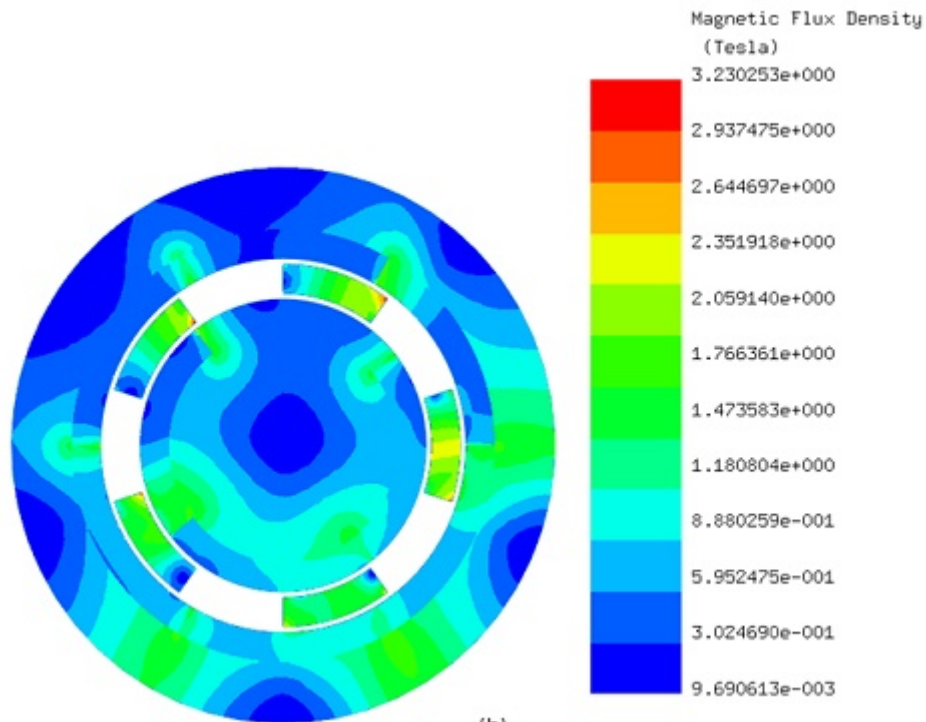


Figure 3 - Plot of the mesh created in EMWORKS 2D

Initially, the LS rotor and ferromagnetic pieces are stationary, while the HS rotor rotates from 0° to 90° . EMWorks2D conducts a parametric sweep to compute magnetic flux and torque relative to the inner rotor angle. Figures 4a) and 4b) show magnetic flux density at $\phi_i = 0^\circ$ and $\phi_i = 52^\circ$, emphasizing high flux concentrations in the ferromagnetic bodies. Figure 5 displays non-uniform flux density in the air gap at $\phi_i = 52^\circ$, influenced by rotor pole positions. Magnetic vector potential lines in Figure 6 demonstrate flux conduction between HS and LS rotor poles via the ferromagnetic pieces, with almost all flux circulating within the device.



(a)



(b)

Figure 4 - Magnetic flux results, a) $\phi_i = 0^\circ$ b) $\phi_i = 52^\circ$

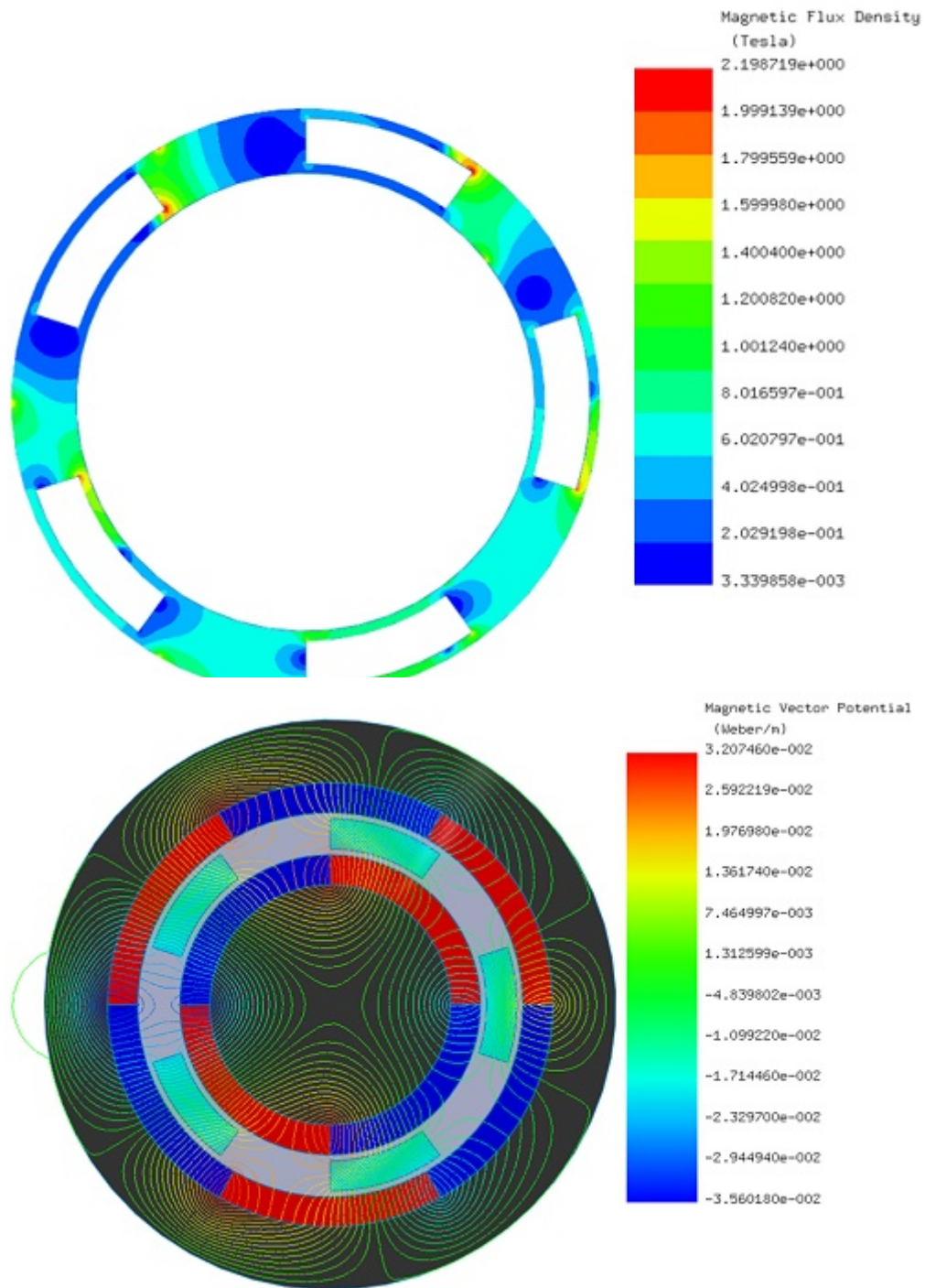


Figure 6 - Magnetic vector potential lines ($\phi_i = 0^\circ$)

Figure 7 shows the magnetic torque generated on the HS rotor while the LS rotor and the ferromagnetic pieces are kept stationary. The torque is nearly null at $\phi_i = 0^\circ$, then it starts increasing with the angle until reaching a first peak of 70 N.m at $\phi_i = 35^\circ$. The torque curve reaches a second peak of 74 N.m at $\phi_i = 51^\circ$, then it drops down until becoming again null at $\phi_i = 90^\circ$.

Figure 7 - HS rotor torque (LS rotor and ferromagnetic pieces are fixed)

Now the generated torques are evaluated when the inner and outer rotors are both rotating in opposite directions (ferromagnetic pieces are fixed).

The outer rotor angle ϕ_o is described using the following equation: $\phi_o = -\phi_i \times \frac{p_i}{p_o}$ [2]. The HS rotor starts at an angle of 40 degrees, resulting in a torque of approximately 62 Nm, while the LS rotor torque is about 98 Nm. Figures 8a) and 8b) illustrate the torques exerted in the inner and outer rotors, respectively. The average torque in the HS rotor is around 67 Nm, compared to nearly 101 Nm in the LS rotor, yielding a gear ratio of approximately 3:2. Consequently, rotating the inner rotor amplifies the torque by 1.5 times in this magnetic gear system.

Figure 8 - Torque results, a) inner rotor, b) outer rotor

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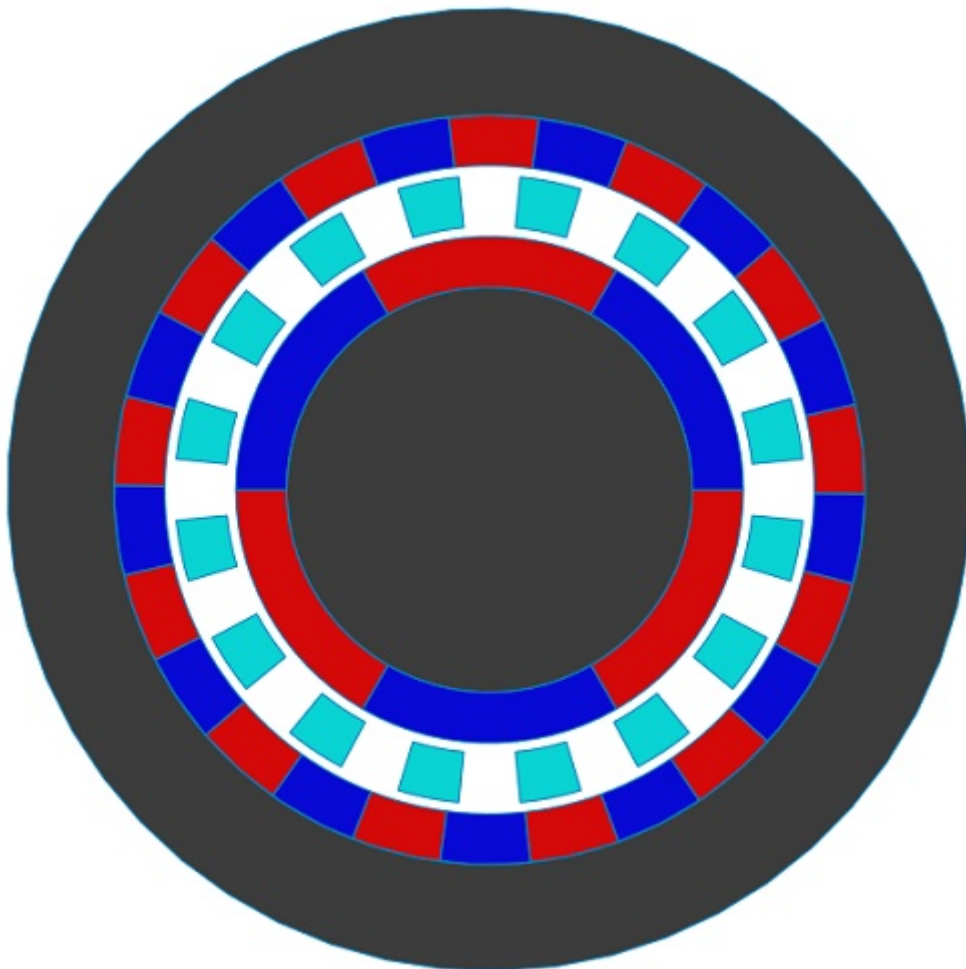


Figure 9 - 2D model of the new magnetic gear system

In Figure 10, the flux lines illustrate how the intermediate ferromagnetic pieces conduct the flux within the air gap region. Moving forward, torque calculations are performed with the HS rotor rotating while the LS rotor and ferromagnetic pieces remain fixed (θ_i varies from 0° to 60°). The resulting torque curve for the HS rotor is depicted in Figure 11, peaking at around 41 N.m at $\theta_i = 30^\circ$. Subsequently, Figures 12a) and 12b) display the torque curves for the inner and outer rotors, respectively, spinning in opposite directions. Notably, the HS rotor produces a torque of 41 N.m, while the LS rotor generates approximately 175 N.m. These torque values align with Figure 12b) where ripp

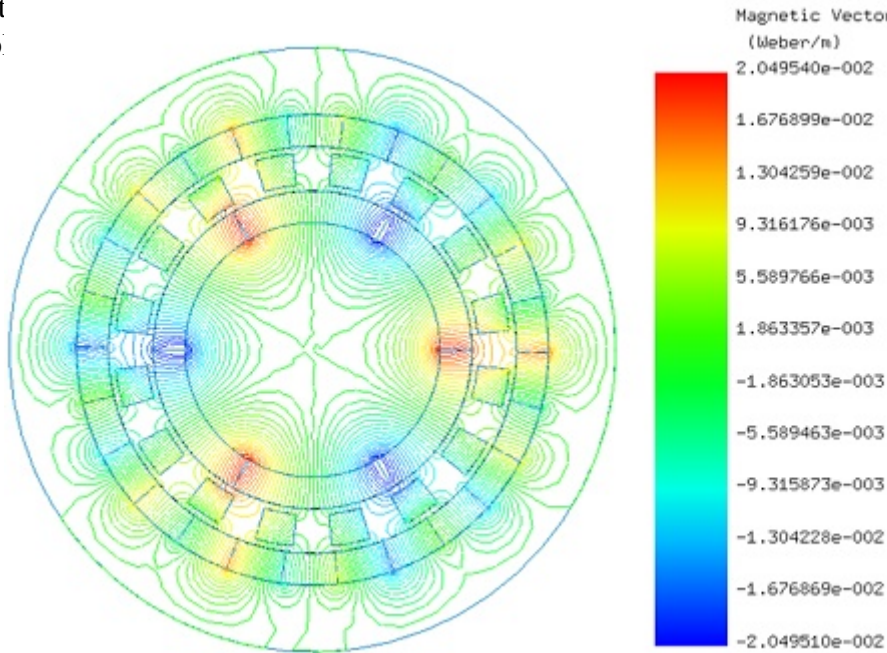


Figure 10 - Flux lines plot

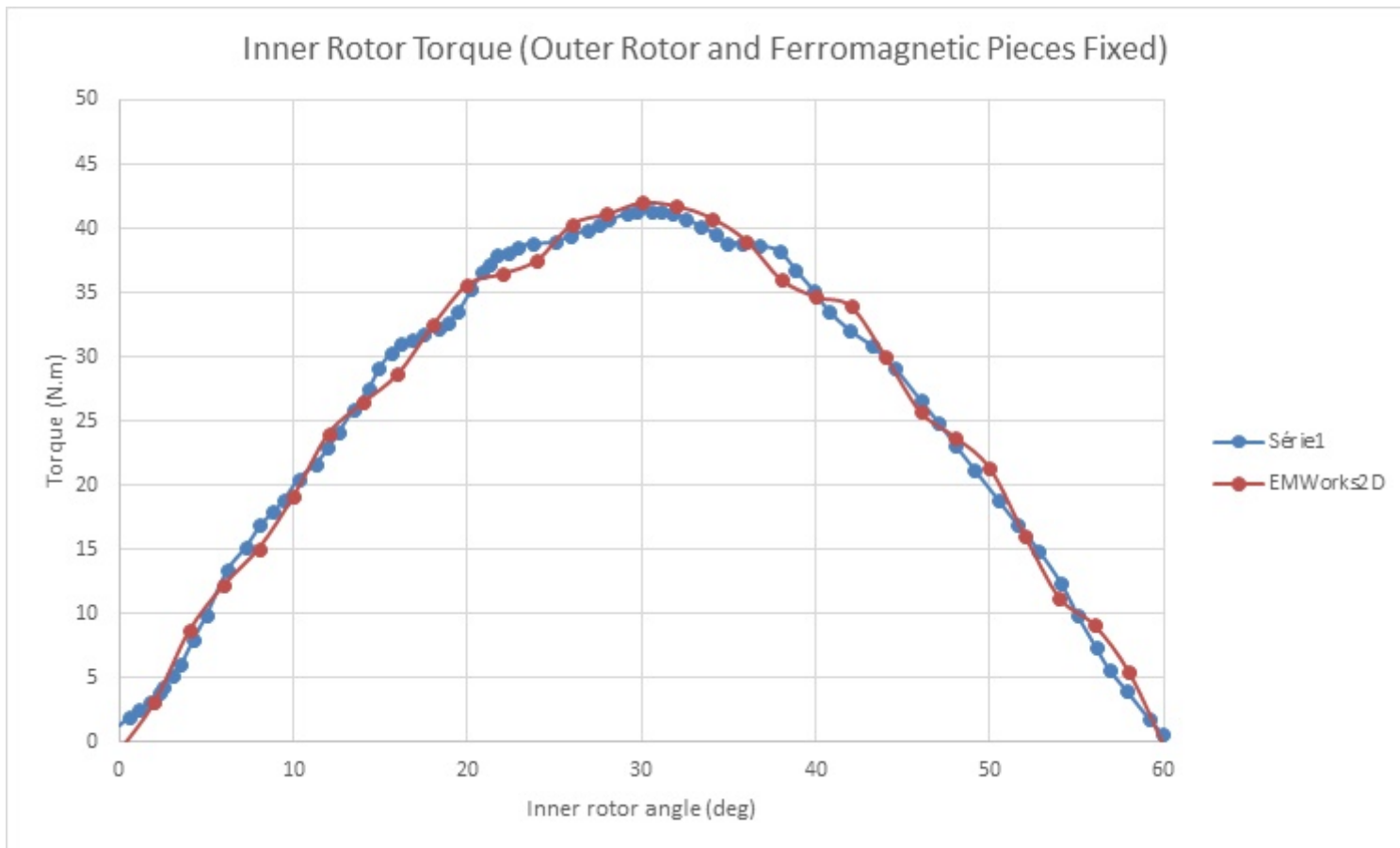


Figure 11 - Inner rotor torque while keeping outer rotor and ferromagnetic pieces fixed

Figure 12 - Torque results, a) inner rotor, b) outer rotor

Conclusion

The application note focuses on magnetic gears, highlighting their advantages over traditional mechanical gears, including frictionless operation, reduced maintenance, and no direct contact, leading to enhanced efficiency and reliability. Magnetic gears are particularly beneficial in environments requiring clean operation and high safety, such as in electric vehicles and industrial machines. The study uses EMWorks2D to analyze two coaxial magnetic gear models, demonstrating how finite element method (FEM) simulations can optimize torque and magnetic flux distribution. Key findings reveal that magnetic gears can effectively transmit high torque without physical wear, showcasing their potential to revolutionize power transmission systems in various applications. This research underscores the importance of design and simulation in advancing magnetic gear technology for future engineering solutions.

References

[1]:P.M. Tlali, R-J. Wang, S. Gerber. *Magnetic Gear Technologies: A Review*. IEEE: 2014 International Conference on Electrical Machines (ICEM)

[2]:Thierry Lubin, Smail Mezani, Abderrezak Rezzoug. *Analytical Computation of the Magnetic Field Distribution in a Magnetic Gear*.

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